

MULTI-SIGNAL DETERMINATION OF POLARIZATION DEPENDENT CHARACTERISTIC

BACKGROUND OF THE INVENTION

The present invention relates to the measurement of optical devices having
5 single or multiple ports and comprising one or more optically active or passive
components. In particular, the invention relates to a determination of
polarization dependent characteristic of these devices.

A method of measuring multi-port optical devices is known from EP-A-1235062.
Testing optically active or passive devices exhibiting polarization dependent
10 characteristic has become an increasingly important task in optical
communications measurement industry. With ongoing increase of distances in
optical transmission communication systems, mechanical stress or temperature
induced birefringence, e.g., in optical fibers, are growingly affecting
polarization characteristic of a signal that is input to the communication system,
15 i.e. to one or more optical devices. Optical devices affected by polarization
changes are among others, e.g., switches, cross-connects, attenuators, fiber
optic couplers, filters, isolators, amplifiers, or passive fiber optic transmission
lines. Changes in the state of polarization of a signal input to optical devices
may result in unwanted signal fluctuations. Characterization of an optical
20 device with respect to polarization therefore is one of the main goals when
improving optical transmission systems. A method of measuring polarization
mode dispersion (PMD) is known from US-A-6,144,450.

SUMMARY OF THE INVENTION

It is an object of the invention to provide an improved testing of optical devices with respect to polarization characteristic. The object is solved by the independent claims. Preferred embodiments are shown by the dependent
5 claims.

An optical device under test (DUT) having at least one input and at least one output is applied with a stimulus signal, which is superimposed with characteristic identification portions, each of said portions being set into a different state of polarization by means of a plurality of polarization units. This
10 stimulus signal is introduced to the system by means of a signal application unit, which - according to a preferred embodiment - may comprise one or more optical signal sources, e.g. a tunable laser source, but the stimulus signal may also be introduced from an external source.

The signal application unit forwards the stimulus signal to each of the plurality
15 of polarization units. Each of said polarization units is designed to set the stimulus signal forwarded from the signal application unit into a unique state of polarization. In particular, a state of polarization set by a first polarization unit differs from another state of polarization set by a second polarization unit.

Polarization units as described in this document may comprise polarization
20 controllers. One known and commonly available product is the Agilent 8169 A polarization controller of the applicant Agilent Technologies. Polarization controllers as being usable in the present system may either be designed to set an incoming optical signal into a fixed state of polarization or may be designed to apply adjustable, variable polarization characteristic to said signal. What is
25 important is, that a single stimulus signal is introduced by the application unit and is applied - or split - towards each of the polarization units, each of said polarization units setting the stimulus signal separately into a unique state of polarization, which differs from that of another polarization unit within the

present set.

In order to enable to recover each of the polarized stimulus signals out of a response signal output from the DUT, a characteristic identification portion is attached to each of the polarized stimulus signals. In other words, one
5 modulation unit affecting said identification portion is each associated with one of the polarization units. A characteristic identification portion within said stimulus signal uniquely corresponds to a state of polarization applied to the signal by means of the polarization unit.

In a preferred embodiment, the stimulus signal as being applied by the signal
10 application unit comprises a carrier portion having a carrier frequency. Said modulation unit is designed to apply the characteristic identification portion by means of frequency, amplitude or phase modulation to a stimulus signal. According to this embodiment, the identification portion is represented by mixture frequencies located in side bands of the carrier frequency.

15 The uniquely polarized and identifiable stimulus signal split towards each of the polarization units is then superimposed for being input to the optical device under test. Accordingly, the superimposed signal comprises a carrier portion having multiple components with differing states of polarization each portion being characterized by one unique frequency.

20 The DUT to be tested with the stimulus signal provided as explained above may have one or more in- and outputs, and may be embodied as any kind of active or passive optical device. Gain systems such as amplifiers, or fiber optic couplers, filters, attenuators, switches, cross-connects, isolators, etc. or even polarization controllers itself maybe examined with respect to polarization
25 characteristic using the system and the method of the present invention. However, the invention is not restricted to devices as listed above, rather the invention is applicable to any device, or system of devices including long transmission line systems, which exhibit polarization change characteristic, in

particular polarization dependent loss, which will be explained in embodiments below.

The response signal associated with the stimulus signal by means of the DUT is received by a signal receiving unit. In a preferred embodiment, the signal
5 receiving unit comprises an optical power meter for measuring the response signal. The signal receiving unit may comprise a semiconductor diode as a sensor element, e.g., InGaAs-diodes for a wavelength range 850 - 1700 nm, Ge-diodes for 600 - 1650 nm or Si-diodes for 400 - 1000 nm.

During transformation of the optical into an electrical signal mixed frequency
10 signals – or so-called beat signals - are generated in the low frequency regime of the side bands of the carrier signal, which have a state of polarization that is not orthogonal with respect to a polarization of a respective other side band signal. The electrical beat signals can now advantageously be separated in the electrical regime by means of suitable electrical filters. By means of
15 appropriate coding, each of the individual frequencies may be associated with one of said states of polarization.

The receiving unit is therefore enabled to trace the identification portion originating from the stimulus signal from within the response signal. Due to the polarization characteristic of the optical device, the polarized identification
20 portions are affected by loss or gain characteristic. With the help of the signal receiving unit, each of the polarized identification portions traced within the response signal can be measured.

According to a preferred embodiment of the invention, the measured values of the polarized identification portions, e.g. the power of each component, is
25 compared each with a value being measured for the same portion with a DUT known not to display a polarization dependent characteristic, e.g. a fiber channel, or else being known prior to entering the device under test. By such a comparison, the loss- or gain-change of the applied states of polarizations

(SOP_x) can be derived. Based on these polarization dependent loss or gain measurements the so-called Mueller-method can be used to evaluate the maximum and minimum signal power and therefrom, e.g., the polarization dependent loss (PDL) or gain (PDG). Such a derivation as well as a detailed analysis is carried out by means of an evaluation unit. The evaluation unit may comprise a PC, workstation or other logical processing unit, the user interface, and/or a memory. A main characteristic of the DUT is the maximum loss-deviation due to polarization change of the input signal maybe represented by the polarization dependent loss PDL (for active optical components, e.g., amplifier a term "positive loss" = gain (PDG) is utilized). The invention becomes most advantageous in a preferred embodiment, according to which the loss characteristic (or gain characteristic) are determined by just analyzing the loss / gain change behavior of four well-defined states of polarization. A matrix, e.g., the so-called Mueller-matrix, is set up relating each of the components of the four states of polarization prior and after passing the DUT to each other. The corresponding linear equation system is then solved by means of the evaluation unit, wherein the polarization dependent loss can easily be represented by the matrix coefficients. An example will be given in the detailed description as provided below.

A main ingredient is that the stimulus signal is split into a plurality of portions, each portion being supplied with an additional identification portion and a unique state of polarization. In the response signal the state of polarization is recovered by means of the identification portion and is then measured. By coincidentally applying, e.g., four or more states of polarization the coefficients can be derived with just one measurement cycle, i.e. a single shot of said stimulus signal. Prior art methods employed serial measurement techniques (in time). Thus, few efforts are necessary; in particular, less time and calibration work is needed to characterize an optical device.

The invention can be partly or entirely embodied or supported by one or more

suitable software programs, which can be stored on or otherwise provided by any kind of data carrier, and which might be executed in or by any suitable data processing unit. Software programs or routines are preferably applied to receive the measured values of the polarized signal components from the response signal, compare each of the components with corresponding values known or measured from the stimulus signal and then solve a linear equation system relating the components to each other.

BRIEF DESCRIPTION OF THE DRAWINGS

Other objects and many of the attendant advantages of the present invention will be readily appreciated and become better understood by reference to the following detailed description when considering in connection with the accompanied drawings. Features that are substantially or functionally equal or similar will be referred to with the same reference sign(s).

Fig. 1 shows a schematic illustration of a first embodiment of the present invention;

Fig. 2 show a schematic illustration of a second embodiment of the present invention;

Fig. 3 shows a signal spectrum with states of polarization each of the stimulus signal and the response signal that is generated by the system shown in Fig. 2.

DETAILED DESCRIPTION OF EMBODIMENTS OF THE INVENTION

Referring now in greater detail to the drawings, Fig. 1 shows a schematic illustration of a first embodiment of the present invention providing a system for determining polarization dependent characteristic of an optical device under test 10 (DUT). According to this embodiment, an optical stimulus signal 6 of a TLS 4 is provided to a first coupler 105. The first coupler 105 has 4 output

ports and splits the optical signal 6 into 4 parts 6a, 6b, 6c and 6d. Each signal part 6a, 6b, 6c and 6d is modulated by modulation units 27, 29, 127 and 129, respectively. The first signal 6a is modulated using a first binary code code 1, the second signal part is modulated using a second binary code code 2, the
5 third signal part is modulated using a third binary code code 3, and the fourth signal part is modulated using a fourth binary code code 4. Codes 1, 2, 3 and 4 are orthogonal to each other.

Subsequently each coded signal 6a', 6b', 6c', 6d' receives a defined polarization by polarization controllers 27a, 29b, 127c, 129d in the path of the
10 coded signal 6a', 6b', 6c', 6d', respectively. The resulting polarized signals 6a'', 6b'', 6c'', 6d'' are then combined at a coupler 135 and provided as a superimposed signal 136 to a DUT 10. As modulation units 27, 29, 127, 129 intensity modulators (e.g. LiNbO₃- based) can be used.

A response signal 140 leaving the DUT 10 is then detected at a detector 44. A
15 detector signal 48 containing coded signals for main polarizations and cross polarization is then provided to a correlation unit 52 containing four correlators 52-1, 52-2, 52-3 and 52-4. Each correlator 52-1, 52-2, 52-3 and 52-4 is demodulating the signal 48 by multiplying signal 48 with the codes code 1, code 2, code 3 and code 4, respectively. The results of the demodulation is
20 then provided by the correlation unit 52 at output ports a, b, c and d of the correlators 52-1, 52-2, 52-3 and 52-4, respectively.

Fig. 2 shows a schematic representation of a second embodiment. An optical stimulus signal S_a is generated by a tunable laser source 4. The wavelength may be tuned over a limited wavelength range in order to investigate
25 polarization effects of DUT 10 that further depend on wavelength.

The stimulus signal S_a is input to a first polarization unit 20, which may be a polarization controller, for setting the signal into a predetermined state of

polarization (signal S_b). This step is performed since optical modulation units such as a Mach-Zehnder based on LiNbO_3 as well as the subsequent polarization units generally work polarization dependent. Consequently, the influence of systematic errors on the measurement results can considerably be reduced. In this embodiment polarization controller 20 polarizes signal S_a linearly with angle 90 degrees. The resulting spectrum is depicted with its attached state of polarization in Fig. 3. The signal attains the form

$$E_{in}(t) = E_0 \cos(\omega_c \cdot t),$$

wherein ω_c is a carrier frequency.

- 10 The resulting signal S_b is then applied in parallel – or split - to each one of a set of modulation units 30-1 ... 30-4. In this embodiment, a set of four modulation units is implemented. These modulation units modulate stimulus signal S_b by means of, e.g., amplitude, phase or frequency modulation. While the spectrum of polarized signal S_b is represented by one or more carrier
- 15 frequencies, the corresponding carrier portion signal S_b is thus supplemented with each an unique identification portion to give modulated stimulus signals $S_{c-1} \dots S_{c-4}$.

For example, a modulation frequency $1 \cdot \omega_m$ is applied to the stimulus signal S_b that enters modulation unit 30-1, and a modulation frequency of $4 \cdot \omega_m$ is applied

20 to the stimulus signal S_b that enters modulation unit 30-2. Modulation units 30-3 or 30-4 apply identification portions with modulation frequencies of $16 \cdot \omega_m$ or $64 \cdot \omega_m$, respectively, to the incoming stimulus signal S_b . These incommensurabilities of the multipliers (1, 4, 16, 64) are chosen such as to inhibit mixture frequencies of different states of polarization when transforming

25 optical signals into electrical signals. Other multiplication values might equally

be chosen, such as (1, 3, 9, 27). An expression for stimulus signal S_{C-1} is given by

$$E_{\text{mod}}(t) = E_0 \cdot (\cos(\omega_C \cdot t) + \frac{m}{2} \cos(\omega_C - \omega_m) + \frac{m}{2} \cos(\omega_C + \omega_m)).$$

Each of the modulated stimulus signals is then forwarded to one of a set of polarization units 40-1 ... 40-4, which each may be embodied, e.g., as a polarization controller. Stimulus signal S_{C-1} is retained in its state of polarization, i.e. linear vertical (90°) polarization. Stimulus signal S_{C-2} is converted to linear diagonal (45°) polarization, Stimulus signal S_{C-3} is converted to linear horizontal (0°) polarization, Stimulus signal S_{C-4} is converted to circular polarization. Each of the four separated stimulus signals S_{C-1} ... S_{C-4} now has a unique pair of modulation frequencies and states of polarization. The polarized, modulated signals are denoted as S_{D-1} ... S_{D-4} in Fig. 3a.

Leaving the set of polarization units 40-1 ... 40-4, the separated stimulus signals S_{D-1} ... S_{D-4} are superimposed prior to being input to said DUT 10. The resulting frequency spectrum of modulated, polarized stimulus signal S_D is depicted in Fig. 3b.

A frequency selective receiver 60 receives a response signal R_a from DUT 10. As explained above said receiver 60 is adjustable in selecting desired frequency ranges by comprising an optical/electrical signal transformation unit (by means of, e.g., a semiconductor diode) with corresponding electrical filters having filter wavelength ranges according to the current needs. Accordingly, it becomes possible to select the identification portion of the transformed signal in order to trace and recover an indication of one of the stimulus signals S_{D-1} ... S_{D-4} within the (electrically transformed) response signals R_{b-1} ... R_{b-4} .

It is clear to a person skilled in the art of optical communications measurement device techniques that instead of using one adjustable frequency selective receiver four or more frequency selective receivers 60 may be employed in parallel, each of them being fed with an input DUT response signal coming from a coupler, which splits the response signal R_a into at least four different parts.

Each signal measured by the power meter 70 (bandpass larger than 2 times the maximum of the modulation frequency) comprises the following frequency dependent characteristic signals:

$$I_{2\omega \text{ mod, pol}}(t) = T_{\text{pol}} \frac{(E_0 \cdot m)^2}{2} \cos(2\omega_m \cdot t),$$

wherein T_{pol} denotes a loss of power for the respective polarized signal (shown in Fig. 3c). By referencing to the previously performed calibration of the input signals, polarization dependent loss or gain coefficients can be evaluated by means of the Mueller method.

PDL is the maximum change in transmission of an optical component versus all possible input polarization states. As E_0 (e.g. by a similar measurement with a power meter prior to inputting the signal into the DUT 10) and ω_m are known and the intensity is measured, the polarization dependent characteristic of the DUT 10 can be derived.

An evaluation unit 80 extracts the measured power values and starts a detailed analysis of these results based on the concept of the Mueller matrix, which describes a transition of states of polarization due to, e.g., an optical element:

The power and state of polarization of an arbitrary signal may be fully represented by the Stokes Vector $S=(S_0, S_1, S_2, S_3)$, wherein S_0 represents the power, S_1 the amount of linear horizontal polarization, S_2 that of $\pm 45^\circ$

- linear horizontal polarization and S3 the amount of left or right hand circular polarization. The relation between the Stokes vector of the stimulus input signal and that of the output response signal can be expressed by a linear equation system which is represented by a 4x4 matrix, also called the Mueller-
- 5 Matrix. For the reason that only the output power with respect each state of polarization is measured by means of power meter 70, and just the polarization dependent loss relating input and output powers to each other is searched for, just four coefficients of the Mueller Matrix are of interest here, i.e. are to be determined when solving the equation system.
- 10 A method of solving the equation system via the Mueller Matrix is provided in Hentschel, C. and Schmidt, S. in: "*PDL Measurements using the Agilent 8169A Polarization Controller*" (Product Note available via internet: <http://cp.literature.agilent.com/litweb/pdf/5964-9937E.pdf>), the content of which is fully incorporated here for reference. In particular, coincidentally measuring
- 15 the four output power values of the response signal and relating them to the known four input powers, the whole state of polarization of the response signal can be characterized, i.e. the output signal Stokes vector can be fully determined in just one shot PDL-measurement.